

Development of Processes for Purification of Coal Processing Gases from Sulphur and Cyanide and the Application in Energy Technologies

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Abstract

For the efficient use of gases formed in a number of thermochemical procedures of carbon processing it is necessary to purify them from hazardous impurities, such as H_2S , HCN , NH_3 , resinous substances. For the purification of the gases, it is proposed to use the liquid catalytic procedure with the soluble derivatives of cobalt hexamethylenetetramine as a catalyst. This method allows achieving the required purification extent with low expenditure. The purified gases can be used to obtain electricity and heat, and also as chemical raw material for obtaining ammonia, methanol, liquid fuel, etc. Elemental sulphur is obtained as a result of purification.

INTRODUCTION

The enormous resource basis of the coal industry of Russia (the first place in the world in respect to coal resources and the third place in the explored resources) allows one to develop a long-term concept of the development of economical coal power engineering and coal processing into chemical products. Thermochemical coal processing (coking, low-temperature coking, semi-coking, gasification, steam and oxygen conversion) results in the formation of the corresponding gases which require purification from hazardous impurities. They can be used as a fuel or as a raw material for producing chemical products (ammonia, methanol, liquid fuel, etc.). The fraction of coal subjected to gasification is likely to increase substantially in the near future, with the

OUTLOOKS OF COAL PROCESSING BY MEANS OF PRELIMINARY GASIFICATION FOLLOWED BY THE PURIFICATION OF THE RESULTING GAS

One of the promising methods of coal processing into electric and thermal energy involves preliminary gasification of the coal followed by purification of the resulting gas from hazardous impurities (sulphurous, nitrogen-containing compounds, gum-like products, soot particles). The advantage of this technology for carbon processing (gasification + purification of the resulting gas) is the possibility of incorporation of the purified gas in gas turbine power plants (GTPP) which allow transforming up to 28–32 % of the heat of burnt fuel into electricity [2]. Incineration in GTPP equipped with boiler-utilizers helps achieving also maximum total utilization of the heat of burnt fuel.

gas at a point below dew point for sulfuric acid, since the waste gas does not contain sulphur oxides. The flue gas will contain solid particles, sulphur or nitrogen oxides. The absence of nitrogen oxides in exhaust gas is achieved thanks to preliminary purification of the gas from nitrogen-containing compounds. In addition, temperature not higher than 1500 °C is maintained in the combustion chamber of GTPP, which prevents the formation of noticeable amounts of nitrogen oxides from nitrogen and oxygen. Such a low temperature of incineration of the gas obtained from coal gasification, unlike natural gas incineration, is possible due to its high hydrogen content.

In addition to high extent of utilization of the heat of burnt fuel (processed coal) and environmental safety, this technology has one more important advantage. Coal gasification and processing of the obtained gas can be performed in different territories: gasification can be carried out close to coal mining or unloading site, and incineration close to the site where electricity and thermal energy are to be consumed. Transportation of the obtained gas along pipeline is possible due to its preliminary purification from hazardous (aggressive) mixtures.

The application of this technology of coal processing into electricity and thermal energy is very urgent nowadays. Because of increasing difficulties in oil and gas production and limited resources (it is assumed that the reserves of natural gas in Russia will be over for the nearest 30–40 years), a substantial decrease in the fraction of coal in the total amount of fuel to be processed into electricity and thermal energy is planned [1]. At the continuation of the existing technologies, growth of coal processing will cause a substantial increase in emissions into the atmosphere. According to the data of RAO "UES of Russia", the increase in NO_x emission by 13 %, SO_x by

100 % will be observed. In order to obtain electricity and thermal energy with the help of gas turbine power plants equipped with boiler-utilizers, one also uses gases obtained by coking, semi-coking, steam and oxygen conversion of coal. Methods are also developed to use poor gas from coal gasification in the existing and specially developed GTPP, including those with the catalytic combustion chambers. This will allow one to process wastes from coal-concentrating plants into electricity and thermal energy. The use of the resulting coal wastes (high-ash coal) for generating electric and thermal energy would allow one to save coal resources not mined, to prevent land disabling by tailings (coal wastes). In addition, one cannot exclude the possibility to use coal wastes accumulated previously (tailings) may account for millions tons near actual coal processing. Previously existing coal concentrating plants.

The major hazardous components in coal processing gases are hydrogen sulphide (H_2S), ammonia (NH_3) and hydrogen cyanide (HCN), which cause the corrosion of equipment during transportation, compression and combustion. Gases obtained by thermochemical processing can be used as chemical raw material or as fuel. H_2S and HCN are the strong catalyst poisons in the synthesis of ammonia, methanol and liquid fuel. During combustion of coal processing gases, these compounds are transformed into not less toxic sulphur and nitrogen oxides.

Amine purification has become the most widespread method of fuel gas purification from H_2S , followed by the processing of resulting acidic gases into elemental sulphur according to Claus procedure. However, the application of amine methods to purification of gases obtained by coal processing is hindered due to the presence of such compounds as H-resins, easily polymerized unsaturated hydrocarbons, nitrogen bases (NH_3), solid particles (ash, coal) [5]. The presence of the listed

tion process (amine purification) utilize of acidic gases according to Claus process) also worsen in the case when installations with low productivity with respect to the extracted H_2S are built, for example, for the purification of low-sulphur gases. In this case, utilization of a substantial part of heat during combustion of acidic gases at the stage of processing according to Claus procedure is impossible. Because of the presence of resin-like and easily polymerized components in gas obtained by carbon gasification, the utilization of adsorption and heterogeneous catalytic high-temperature purification processes is also hindered.

In order to purify gases obtained by thermochemical coal processing, the methods of purification from sulphur and sulphur-cyan purification existing at present or being under development can be recommended, since they take into account that the gas under purification contains HCN, NH_3 , unsaturated hydrocarbons, resin-like compounds in addition to H_2S . In the world industry, more than fifteen variations of technological processes of coke gas purification have been introduced [6, 7]. Such diversity is due to the differences in the composition of coked mixtures and therefore in the composition of the coke gas, and also due to different requirements to purification extent and to resulting products. Oxidative purification methods involving liquids (wet processes) are widespread. The processes of wet oxidative sulphur- and cyan purification (Hols-Stretford, Fumax-Rodax, Takahacs-Hairman) providing high degree of gas purification from H_2S and HCN (up to 99.9 %) [4] are not widespread in Japan, Great Britain and Canada. The essence of these processes is reduced to the absorption of acidic components of coke gas by ammonia or soda solution. After that, catalytic oxidation of the absorbed hydrogen sulphide to sulphur is performed in solution, and the catalyst is recovered by blowing air through the solution. The processes are

are preliminarily purified from resinous substances and from hydrogen cyanide. For hydrogen sulphur gases obtained by coal processing, preliminary purification from HCN is economically efficient, because large amount of commercial high-quality sulphur is obtained as a result of subsequent purification of gas from HCN. The resulting water-wetted sulphur can be used as a fungicide [7].

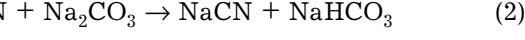
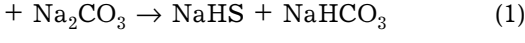
DEVELOPMENT OF PROCESSES FOR THE PURIFICATION OF COAL PROCESSING GASES

A specific feature of gases obtained by thermochemical processing of eastern coal is the high content of sulphurous compounds (H_2S) and HCN. As a consequence, low H_2S /HCN ratio (usually H_2S /HCN = 1, which makes it economically unreasonable to purify the gas separately: first from HCN, and then from H_2S . It is desirable to perform simultaneous purification of sulphur gases from hydrogen sulphide and from hydrogen cyanide obtaining thiocyanates. In order to avoid accumulation of these salts in solution, either intensive drainage or frequent replacement of absorbing solution is necessary, so the absorbing solution should be rather cheap. Requirements to the level of admixture of HCN in gas, which are able to get accumulated in the absorbing solution, can be made not so strict, because absorbing solution will be often replaced.

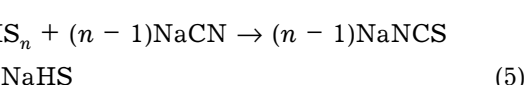
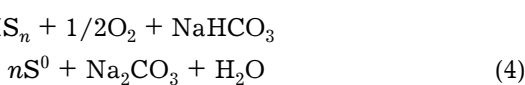
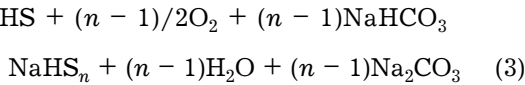
For low-sulphur coke gas, a catalytic liquid-phase oxidative method of simultaneous purification from H_2S , HCN and resin-like substances has been proposed, with soluble derivatives of cobalt phthalocyanine (CoPc) as a catalyst [8, 9]. Cobalt phthalocyanine and its water-soluble derivatives are characterized by high activity in liquid-phase oxidation of hydrogen sulphide by oxygen in alkaline medium. Due to high activity, the concentration of phthalocyanine catalysts in absorbing solutions can be very low (several milligrams per litre), which pro-

containing an alkaline reagent (Na_2CO_3 , KOH , NaOH) and a catalyst, which is a soluble phthalocyanine derivative in monomeric [9] or polymeric form [8]; this results in absorption of gaseous admixtures: H_2S , HCN and resinous substances. The saturated absorbing solution is then blown with air at the regeneration stage; this is accompanied with catalytic oxidation of the absorbed hydrogen sulphide, which is present in solution mainly in the form of HS^- ions, by the dissolved oxygen. As a result of the oxidation, depending on conditions, different products can be formed: elemental sulphur, thiosulphates, sulphites, sulphates [10, 11]. During the simultaneous purification of the gas from H_2S and HCN , it is necessary to obtain elemental sulphur along with thiocyanates. The main intermediate product of the oxidation of HS^- ions to sulphur is polysulphide ion. The presence of freshly formed elemental sulphur and polysulphide ions in solution allows hydrogen cyanide absorbed from gas to be transformed rather rapidly into thiocyanates [12]. The following reactions proceed under the optimal mode of the process of simultaneous purification of gas from H_2S , HCN and resinous substances:

at absorption stage



at regeneration stage



The purification results in the formation of thiocyanates and elemental sulphur. The worked out process is processed to obtain H_2S , which is

gas from sulphur and cyan were mastered using the liquid-phase oxidative purification of low-sulphur gas. The tetrasodium salt of 2, 9, 16, 23-tetrasulphate of cobalt phthalocyanine (CoTSP), which is one of highly active and best investigated solid catalysts, derivatives of phthalocyanine, as a catalyst for the oxidation of HS^- ions [10, 11, 13–16].

The available literature data and our experimental results obtained in the investigation of the mechanism of the catalytic action of CoTSP in liquid-phase oxidation of hydrogen sulphide by oxygen [10, 11, 13–18] allowed us to establish the main parameters of the oxidation of absorbed hydrogen sulphide at the stage of its oxidative regeneration (pH, composition of the absorbing solution, catalyst concentration).

Selection of optimal pH of absorbing solution

The following guidelines were followed when choosing the optimal pH of solution:

1. High yield of sulphur as a result of the oxidation of HS^- ions by oxygen is observed as a result of the oxidative-reductive transformation of the catalyst: $[\text{Co(II)TSP}] \rightarrow [\text{Co(I)TSP}]_2$ [15]. In the case of the formation of complexes of the catalyst with oxygen ($[\text{CoTSP} \cdot \text{O}_2]$ and $[\text{O}_2 \cdot \text{CoTSP} \cdot \text{O}_2]$) [16], prevailing formation of oxygenated sulphur compounds (sulphites, sulphates) is observed during the oxidation of HS^- ions. An increase in pH of solution helps stabilizing the oxygen complex of CoTSP [17] thus decreasing the yield of elemental sulphur and increasing the yield of oxygenated sulphur compounds.

2. With an increase in pH of solution, the rate of non-catalytic oxidation of polysulphide formed according to reaction (3) increases. Instead of reaction (4), oxidation of polysulphide ions by oxygen proceeds with the formation of sulphites and sulphates.

3. At $\text{pH} > 9-10$, disproportionation of the formed elemental sulphur is observed:

oxidation of HS⁻ ions, which, in turn, ensures a high extent of gas purification from HCN and the formation of thiocyanates. On the other hand, a decrease in pH can sharply decrease the sulphur-absorbing capacity of the absorbing solution. Because of this, it is necessary to choose optimal pH.

Choice of optimal composition

The absorbing solution

Methods to maintain this composition

When choosing optimal composition of the absorbing solution, we took into account the effect of different compounds present in solution on the activity and selectivity of the CoTSP catalyst toward sulphur in the liquid-phase absorption of hydrogen sulphide.

The absorbing solution can contain either compounds absorbed from the coke gas or compounds that are formed during purification from sulphur and cyanide, and accumulated in the absorbing solution. In addition to the catalyst and alkaline agent, the absorbing solution contains the captured hydrogen sulphide (HS⁻) and hydrogen cyanide (CN⁻), freshly formed elemental orthorhombic sulphur, thiosulphate, sulphite, sulphate and thiocyanate ions (sodium (ammonium)). The effect of all these compounds on the catalytic liquid-phase oxidation of hydrogen cyanide in the presence of CoTSP was studied in [19–22]:

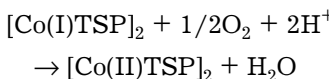
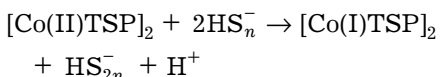
a) The presence of elemental sulphur and sulphates helps increasing the yield of sulphur as a result of oxidation [22];

b) Thiocyanates and sulphates have only a weak effect on the properties of CoTSP catalyst [22];

c) Sulphite and cyanide ions are strong inhibitors [20–22].

The activity of the CoTSP catalyst and its selectivity toward sulphur decrease sharply in the presence of sulphite and cyanide ions. Their inhibition is due to rapid reactions:

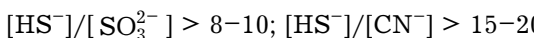
HS⁻ ions by oxygen according to the polysulphide mechanism. Not a slow reaction between the catalyst and HS⁻ ions occurs during the process but a rapid interaction of the catalyst with HS_n⁻ ions:



Realization of the polysulphide mechanism allows conducting the oxidation of HS_n⁻ ions by oxygen at a high rate and high sulphur yield.

Cyanide ions not only destroy polysulphide but also directly affect the catalyst causing inhibition of the oxygen complexes [23] and promoting slower and deeper oxidation of HS⁻ ions by oxygen, which results in the formation of oxygenated sulphur compounds: sulphite and sulphate [11].

The method of simultaneous purification of low-sulphur coke gas from H₂S and HCN using a soluble derivative of cobalt phthalocyanine as a catalyst provides limitation of the accumulation of sulphite and cyanide ions in the absorbing solution. Concentrations of SO₃²⁻ and CN⁻ ions should be rather low, so that the following relations between the concentrations of HS⁻, SO₃²⁻ and CN⁻ ions in the solution entering the stage of oxidative regeneration should be fulfilled:



Low concentration of sodium (ammonium) sulphite is maintained in the absorbing solution due to the presence of suspended freshly formed elemental sulphur (1–5 g/l) and, in addition, due to exposure of the saturated absorbing solution for a definite time (10–20 min) under anaerobic conditions; increased temperature is desirable (40–50 °C). This exposure causes more complete transformation

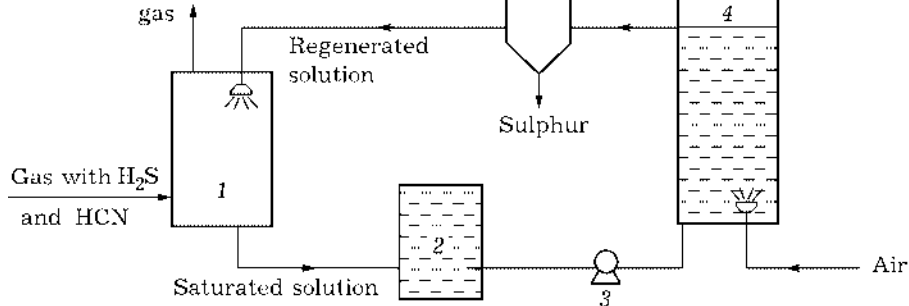


Fig. 1. Scheme of simultaneous purification of the gas from hydrogen sulphide and hydrogen cyanide: 1 - absorber, 2 - reactor, 3 - circulation pump, 4 - regenerator.

A scheme of the set-up for the purification of coke gas from sulphur and cyan is shown in Fig. 1. The set-up includes three major devices: absorber 1, reactor 2, and regenerator 4. The most complete transformation of the absorbed hydrogen cyanide into thiocyanate ions occurs in the reactor. Oxidation of the absorbed hydrogen sulphide into elemental sulphur proceeds in the regenerator.

Selection of optimal catalyst concentration

When choosing optimal catalyst concentrations, we started from the fact that high yield of elemental sulphur as a result of oxidation is observed at a very high rate of the oxidation of HS^- ions in the diffusion region of oxidation process, when $[\text{O}_2]_{\text{sol}} \ll [\text{O}_2]_{\text{equal}}$. As a rule under these conditions high $[\text{HS}_n^-]/[\text{O}_2]_{\text{equal}}$ is observed. For the optimal catalyst concentration, due to very high rate of HS^- oxidation into HS_n^- in solution,

the inhibiting action of SO_3^{2-} and CN^- ions is substantially suppressed [21, 22].

RESULTS OF COKE GAS PURIFICATION FROM SULPHUR AND CYAN BY THE CATALYTIC METHOD

Tests were carried out with the experimental set-up of coke gas purification at the Kemerovo industrial enterprise "Khimprom". The productivity of the set-up was 200 nm³/h. The TSFK catalyst [24] was used, in which the active component is tetrasodium salt of 2,9,16,23-tetrasulphonate cobalt phthalocyanine ($\text{CoPc}(\text{SO}_3\text{Na})_4$ or CoTSP). Coke gas under conditions of purification contained CO_2 2.2–2.5 % vol., H_2S 0.15–0.30 % vol., and HCN 1–2.5 g/m³.

As a result of uninterrupted operation of the set-up for 7 months, optimal parameters of the purification process were established. The required gas purification degree was achieved (residual H_2S <20 mg/m³). With the same

TABLE 1

Results of the purification of coke gas from H_2S and HCN with the experimental set-up at the Kemerovo IE "Khimprom" using the catalytic and arsenic-soda procedures

| Purification parameter | Procedure | |
|---|--------------------------------|--------------|
| | catalytic (with TSFK catalyst) | arsenic-soda |
| Gas consumption, nm ³ /h | 100–125 | 90–110 |
| Specific irrigation, m ³ of liquid per m ³ of gas | 0.03 | 0.04 |

method were performed. Results of the comparative tests are shown in Table 1 [25].

Thus, the method of simultaneous purification from sulphur and cyan has proved to be efficient for purification of low-sulphur coke gas. After minor revisions, this procedure can be used to purify other gases obtained by thermochemical processing of eastern coal; the purified gases can then be used to obtain electric and thermal energy, including incineration of the purified gases in gas turbine power installations.

Complete conversion of the absorbed H_2S to the oxidation products is achieved at the expense of oxidative regeneration of the absorbent solution. Because of this, very low H_2S content can be achieved in the purified gas by varying H_2S absorption conditions at the stage of absorption (a decrease in gas/liquid consumption ratio, involvement of counter-flow). Under definite conditions, almost complete purification of the gas from H_2S is achieved (residual H_2S content $<1-2 \text{ mg/nm}^3$). The purified gas can be used as a raw material to produce ammonia, methanol, liquid fuel.

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